

1 **Towards a Renewal of Transmission & Distribution Infrastructures to meet EU 2020 goals**

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I. Introduction

The month of December 2008 marks an important date in European action against climate change, since the so-called ‘triple 20s’ integrated energy and environmental policy has been adopted by European Commission to strengthen the application of the Kyoto Protocol [1]. Such policy is aimed at setting Europe on the right track towards a sustainable future with a low-carbon, energy-efficient economy by:

- cutting greenhouse gases by 20%;
- reducing energy consumption by 20% through increased energy efficiency;
- meeting 20% of EU energy needs from renewable sources.

The idea is that all nations in Europe will be forced to alter their industrial systems so that they fit to the requirement on carbon reduction and increasing demand on renewable energy by year 2020.

Many studies on such topic have been carried out by Universities and Research Centres, Electrical Companies, International Agencies for Energy Saving and International Workgroups [2 – 4].

As far as the T&D infrastructures are concerned, it should be noted that they are both directly and indirectly involved in the efficient use of energy at any stage. In particular, the following intervention strategies can be identified for the networks modernization:

1. Replacement/refurbishment of power components;
2. Wide area measurement, monitoring and control systems (WAMS/WACS), upgrading protection and control devices for communication;
3. Increase of voltage level;
4. Installation of power quality devices (Distribution Networks);
5. High voltage direct current transmission systems – HVDC (line and forced commutated);
6. Flexible ac transmission systems – FACTS (Transmission Networks).

In this paper, a methodology is proposed to evaluate the impact of the aforementioned actions on the power grids in terms of possible beneficial effects in the context of EU ‘triple 20s’ integrated energy and environmental policy. Such methodology is based both on the identification of suitable “performance (technical) indices” to be used to rank the benefits brought by the different grid upgrading measures and on the definition of suitable “test networks”, which can be employed as benchmarks to perform the numerical evaluation of the introduced indices. Then, a procedure is presented in order to determine and compare the quantitative effect of each single corrective action on T&D power grids. Finally, some considerations on possible side effects and advices on strategies for the implementation of the corrective measures are discussed.

II. Performance Indices to Rank T&D State-of-the-Art Technologies Impact

As already mentioned, the EU energy targets for the year 2020 include improved efficiency, improved environmental compatibility, basically linked to CO₂ emissions reduction and improved renewable generation.

In order to perform a more comprehensive analysis of the possible beneficial effects (environmental + functional) provided by renewing actions on T&D infrastructures, it is possible to integrate these targets with the additional concept of quality of service.

Table I proposes a possible “technical translation” of such targets into the electrical domain. The electrical performance indices can be defined in several forms. The first one is a short term (instantaneous) approach, translated in technical merit, which evaluates the benefits of the introduction of T&D state-of-the-art (modern) technologies mainly in terms of energy per time

76 units, which is power, or electrical aggregated flag quantities. The second way can be
 77 considered as an integral approach (energy), to be computed on a specified time frame, which
 78 proves liable to be converted in an economical merit, such as simple payback time. This
 79 approach includes accurate estimation of investment costs for any additional device to be
 80 proposed. The third approach embraces also probabilistic concepts, particularly useful to rate
 81 dynamic performance indices. A complete evaluation should be based on all the three
 82 approaches; in spite of this, here the choice has fallen into the first one, since it is the most
 83 straightforward and does not require the collection of a large amount of data.
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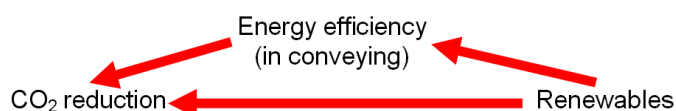
85 **TABLE I**
 86 **DEFINITION OF ELECTRICAL PERFORMANCE INDICES**

T&D EU ENERGY TARGETS	TECHNICAL INDICES
Efficiency	Branch steady state indices (losses containment)
CO ₂ reduction	Generation planning and operation planning (unit commitment – dispatching)
Renewables	
Quality in transmission	Node steady state indices (voltage within limits)
	Dynamic indices (time behaviour compatible with grid protection intervention curves; load shedding, out of step)
Quality in distribution	Node steady state indices (voltage within limits)
	Harmonic indices (Harmonic Distortion Factors)
	Dynamic indices (time behavior compatible with grid protection intervention curves; voltage dips, sags, swells, interruptions)

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89 **II.A Index for efficiency**

90 Energy efficiency should concern with the whole process of energy assessment from power
 91 plant conversion to final user exploitation. The concept of efficiency, in the broadest sense, is
 92 significantly linked to the availability and localization of primary resources, as well as to their
 93 being low cost and/or renewable. If the focus is centered on the electrical segment of the energy
 94 transferring process, we should therefore account for specific efficiency in Generation
 95 (introducing highly efficient generators) ; Utilization (profiting of highly efficient motors and
 96 drives); Energy conveying (usually proposed in terms of loss reduction, but extendable to
 97 power quality).

98 As far as Energy convey is concerned, efficiency in conveying energy implies CO₂ emission
 99 reduction, since losses containment at constant load profile requires less generation amount
 100 (Fig. 1).



101
102 **Fig. 1. Conceptual interdependencies between EU targets at constant load profile.**
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105 At the same time, renewables connected in distribution grids as Distributed Energy Resources
106 (DER) contribute to decrease current circulations and therefore enable reducing Joule losses
107 and improving energy efficiency. Again, renewables adoption results in CO₂ diminishment,
108 since the same load is satisfied by less polluting sources.

109 The proposed index for efficiency is related to the goal of electrical grid losses containment:
110 efficiency and losses containment coincide if constant load profile is assumed.

111 A steady-state model for each branch connection is therefore necessary, and a comprehensive
112 analytical evaluation of complex losses is required; at the same time, steady-state models for
113 specific present state-of-the-art technologies are available and/or ready to re-elaborate from
114 literature, just in order to assess their effect on component efficiency.

115 It should be noticed that different approaches have to be followed in dealing with transmission
116 and distribution grids: in the former, state-of-the-art technologies redistribute flows and losses
117 but ask for a new production profile (dispatching scenario) from all committed power plants.
118 Conversely, in the latter infrastructure, redistribution of flows and losses does not include the
119 modification of generation profile, since DER is not usually asked a load following service, but
120 interconnection to EHV/HV transmission grid acts a power balance compensation system
121 (slack bus).

122 State-of-the-art technologies could otherwise affect DER penetration level by relaxing
123 constraints or improving margins, therefore modifying the overall generation mix.

124 On the basis of such considerations, the performance index for energy efficiency can be thus
125 defined as “*Network losses normalized to total load request*”.

126 The computation of grid total complex losses can be carried out according to Kron-Early loss
127 formulas [5 – 6], which are easy to implement within classical Optimal Power Flow (OPF)
128 formulations.

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130 ***II.B Index for CO₂ reduction***

131 The problem of environmental compatibility of electric power infrastructures is mainly related
132 to the emissions associated to the energy conversion process at the generation stage. Correct
133 management of the interconnection facilities may result in a more environmental friendly
134 scenario, since it could enable commitment of units characterized by reduced CO₂ emission or
135 pushing these units to their maximum possible production capability.

136 The same steady-state model use in subsection A. for any state-of-the-art technologies become
137 useful also to rate their effect on network complex losses amount, since efficiency in conveying
138 energy implies CO₂ reduction.

139 The possible performance index for CO₂ emission can therefore be the “*Total grid CO₂*
140 *emissions normalized to total load demand*”.

141 This is the computation of an optimal generation profile which minimizes greenhouse pollution
142 profile, having previously determined a reliable analytical dependence of emissions on
143 produced power. These optimization procedures enable to account for grid total losses via
144 Kron-Early loss formulas [5 – 6] and for generating unit and grid constraint by means of
145 Kuhn-Tucker conditions [7], which act as penalty factors. From a conceptual point of view, it is
146 a widely adopted energy management procedure, this time extended from minimization of fuel
147 costs to the maximum containment of greenhouse emissions potential of the generation set.

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149 ***II.C Index for renewables penetration***

150 Conveying energy from sites of renewable production to final users is presently an arduous task
151 to face in the modernizing process of the electrical power infrastructure. Time-varying
152 generation profile, as well as development of renewable power in-feed, pose significant
153 challenges in electrical network configuration and management: it sometimes occurs that the

154 infrastructure itself, or its control and protection features, are not ready to completely host
155 renewables access, asking for reconfiguration at several levels.

156 In order to define an index for renewables penetration, again steady-state model for specific
157 T&D state-of-the-art technologies are required to rate the effect of renewable DER on complex
158 losses. As shown in Fig. 1, efficiency in conveying energy is indeed affected by renewables,
159 but state-of-the-art technologies could contribute to improve renewables percentage with
160 respect to the total admissible generation set.

161 The proposal for an index for renewable penetration is then the ***“Total generation from
162 renewables normalized to total load request”***.

163 This index requires the use of optimization techniques, either at unit commitment or generation
164 scheduling level, where cost-production functions are needed for all the installed generation
165 and being the renewables’ ones equal to zero. State-of-the-art technologies affect both grid total
166 losses (again computed via loss formulas) and branches constraints (again expressed via Kuhn-
167 Tucker conditions and reported in terms of penalty factors).

169 ***II.D Index for steady-state quality in transmission and distribution grids***

170 The electric power infrastructure satisfactorily fulfils its tasks if operated in normal conditions,
171 where components and devices are typically characterized by their rated values, fixed by
172 manufacturers to meet best exploitation and duration targets. Any deviation from such profile is
173 paid in terms of a performance reduction. Therefore, it is common interest to limit
174 discrepancies from ideal working scenario, basically related to node voltages and branch
175 currents.

176 As a preliminary proposal for a steady-state quality index, attention is mainly focused on
177 voltage, according to the present operating practice proposed by utilities all around the world.
178 Tolerance in component correct working allows maximum voltage magnitude deviations of 5%
179 in steady-state conditions thus limiting narrower than corresponding (minimum and maximum
180 voltage) protection settings.

181 The evaluation of voltage grid profile requires a steady-state analysis of the electrical system,
182 usually performed via the so-called power flow computation. The steady-state models for
183 specific T&D state-of-the-art technologies is again useful for inclusion in the power flow
184 simulation, leaving a direct chance to detect the relevant modified voltage profile.

185 Investigation on this point reveals that the concept of system adequacy, that is the assessment
186 of a robust operating condition with respect to credible perturbations, must be extended to other
187 flag quantities, like for example branch currents. Current magnitude must not exceed an
188 overload limit, after which a control centre operator intervention is required.

189 Most of the commercial simulations tools consider node voltage and branch current limits in
190 the final violation report, without affecting calculation process. Probably, an improved version
191 of power flow analysis could include such additional constraints in the solution procedure.

192 In light of these considerations, the proposal for a steady-state quality index is the ***“Total
193 mismatch from ideal uniform node voltage and branch rated current profile”***.

194 This requires the computation of an adapted OPF, where the function to be minimized is the
195 sum of node voltage and/or branch current deviations from the ideal working scenario.

197 ***II.E Index for distribution harmonic power quality***

198 Voltage and current waveforms must respect quality standards in order to avoid malfunctioning
199 of end user sensible apparatuses. Time-varying, non linear and discontinuous working
200 components often represent a threat in preserving ideal behavior at the so called points of
201 common coupling, meaning nodes where specific quality constraints are set for contractual
202 reasons. Both converters and unsymmetrical components negatively affect voltages and

203 currents especially at the distribution level, imposing the use of mitigating devices to contain
204 harmonic pollution.

205 As a first proposal for an index for distribution harmonic power quality, one can think at the
206 Harmonic Distortion Factors (HDF), linked to node voltages and branch currents, in terms of
207 indicators of the distance between actual and ideal waveforms. The basic idea considers the
208 definition of harmonic distortion limits, according to residential and industrial context,
209 followed by the use of the harmonic power flow to evaluate HDF in every node and branch.
210 The role played by specific T&D state-of-the-art technologies requires the formulation of their
211 harmonic model and the computation of harmonic distortion in the modified distribution
212 system.

213 The current proposal for the harmonic power quality index is therefore: the “*Network total
214 harmonic (node voltage, branch current) distortion factor average or variance*”.

215 It is included the computation of a conventional harmonic power flow and the evaluation of the
216 sum of all node HDFV and of all branch HDFI, normalized respectively to the n nodes and the
217 b branches inside the distribution grid.

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219 ***II.F Index for transmission dynamic quality***

220 Quality of service is often referred in its steady-state meaning, whereas it becomes difficult to
221 uniquely express a satisfactory transient performance of the electrical power infrastructure.
222 Probably, the most reliable quantity to evaluate should be the system energy, but its definition
223 and computation is far from being elementary and shared. Here, we propose to compare the
224 dynamic evolution of the grid under investigation with the intervention characteristics of the
225 protection devices operating at the transmission level, so that cascading phenomena due to a
226 single event are considered as the main problems to overcome.

227 According to such an approach, a first proposal for the transmission dynamic quality could be
228 related to the comparison between system time behavior and the intervention curves of the
229 installed protection devices. To do this, grid component dynamic models are required, and the
230 installed control loops as well; in addition, credible contingencies have to be defined and it is
231 necessary to identify also the protection set to be considered within this analysis. Then,
232 transient stability simulations can be proposed to assess grid dynamics and capability to recover
233 a correctly operating working point. Dynamic and control models are expected for specific
234 state-of-the-art technologies, so as to include them in the transient stability simulation and
235 evaluate their impact on the system evolution.

236 Being aware of the quantities able to express unacceptable dynamic condition at the
237 transmission stage, which essentially consist in voltage and current magnitudes, frequency
238 deviations and angle displacements, the index for transmission dynamic quality can therefore
239 be defined as the “*Network cumulative proximity to starting thresholds of line distance
240 relays (voltage, current and angle phenomena) and load shedding relays (frequency
241 phenomena)*”.

242 This requires the computation of transient stability and the following monitoring of trajectories
243 in terms of impedances at every transmission line ends and of frequency at every transmission
244 bus bars.

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246 ***II.G Index for distribution dynamic quality***

247 Distribution system dynamics is usually related to instantaneous deviations of voltage
248 waveforms at each point of supply, again a typical contractual clause to be met to avoid
249 penalties. At the present penetration level of distributed generation, electromechanical
250 dynamics is of minor concern, even if liable to become increasingly interesting in the future.
251 Voltage dips, sags, swells and interruptions are detectable as typical phenomena in a short term

252 time frame and represent a frequent cause of economical and physical damage for the final
 253 user.

254 With regard to the just outlined occurrences, the first proposal for a distribution dynamic
 255 quality index is centered on the compatibility of the system time behavior with grid protection
 256 intervention curves, basically linked to over-currents and under-voltages. Such an approach
 257 requires the collection of network components dynamic models, associated to the available
 258 control modes, as well as the definition of credible contingencies and protection systems
 259 operating at the distribution level. Then, a computation of electromagnetic transient and short
 260 circuit simulations is expected, in order to either validate the actual system design or identify its
 261 evident weaknesses. Dynamic and control models for specific state-of-the-art technologies are
 262 subsequently necessary, in order to assess their impact on the dynamic profile of the
 263 distribution grid. According to these considerations, the proposal for distribution dynamic
 264 quality index becomes the “*Network cumulative proximity to ideal voltage and current
 265 waveforms (in case of dips, sags, swells)*”, and the “*Network cumulative unsupplied energy
 266 (in case of interruptions)*”.

267 This requires the computation of electromagnetic transients and the relevant monitoring of
 268 voltage and current waveforms for generic disturbances, whilst an additional time computation,
 269 starting from outage instants at customer supply point, in case of interruptions is required.

270 Table II summarizes the proposed performance indices for each considered objective.

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TABLE II
 TARGETS AND RELEVANT PERFORMANCE INDICES

Target	Performance index
Efficiency	Network losses normalized to total load demand
CO ₂ reduction	Total grid CO ₂ emissions normalized to total load demand
Renewables rate of penetration	Total generation via renewables normalized to total load demand
Steady-state quality in transmission and distribution grids	Total mismatch from ideal uniform node voltage and branch rated current profile
Distribution harmonic power quality	Network total harmonic (node voltage, branch current) distortion factor average or variance
Transmission dynamic quality	Network cumulative proximity to starting thresholds of line distance relays (voltage, current and angle phenomena) and load shedding relays (frequency phenomena)
Distribution dynamic quality	Network cumulative proximity to ideal voltage and current waveforms (dips, sags, swells) Network cumulative unsupplied energy (interruptions)

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III. Test Networks

All the main components of a typical grid must be modeled in the test-network in order to represents their impact on the system performance and also the interaction with other components, such as large generators, Distributed Energy Resources (DER), renewables, distribution transformers, large, concentrated, industrial loads, or residential “distributed” loads.

Several test systems can be found in literature with reference to different specific topics under investigation. In [8] a benchmark network for simulation of FACTS devices in load flow control is presented. In [9], a part of a 20 kV distribution network in a rural area is represented as a “micro-grid”. This system has been used in a pilot project to establish how a network can be operated with a large amount of non-dispatched power sources.

A scheme of a test network potentially useful for the analysis of the previously defined indices is depicted in Fig. 2.

The main characteristic of the system are:

- Minimum number of nodes;
- Division into two sub-systems at two main voltage level;
- Availability of HV-MV transformer;
- Availability of both meshed and radial topology;
- Availability of generation sources at different locations;
- Availability of load at different locations.

Here, we decide to identify all T&D systems and components by resorting to suitable generalized circuital representations, able to describe different technologies and solutions, according to the parameters choice.

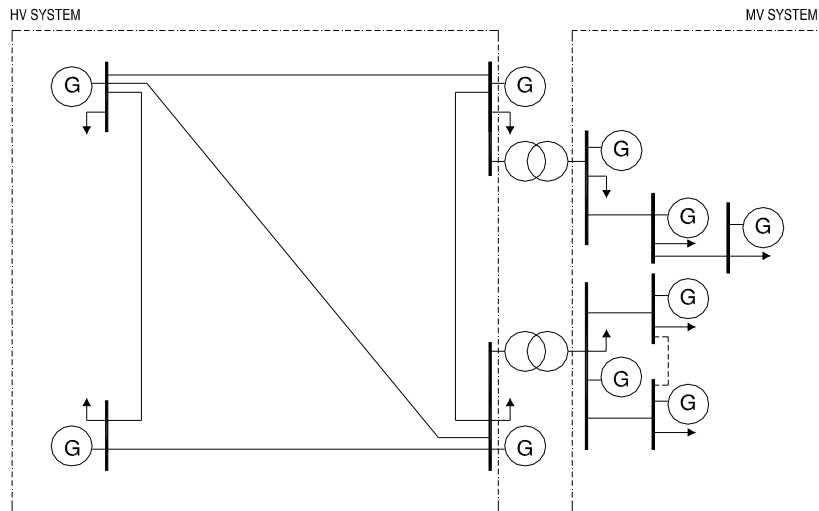


Fig. 2. HV-MV network for the evaluation of performance indices.

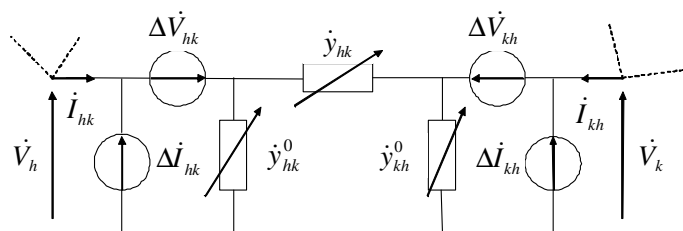


Fig. 3. Generalization of T&D state-of-the-art technologies in families: steady-state model.

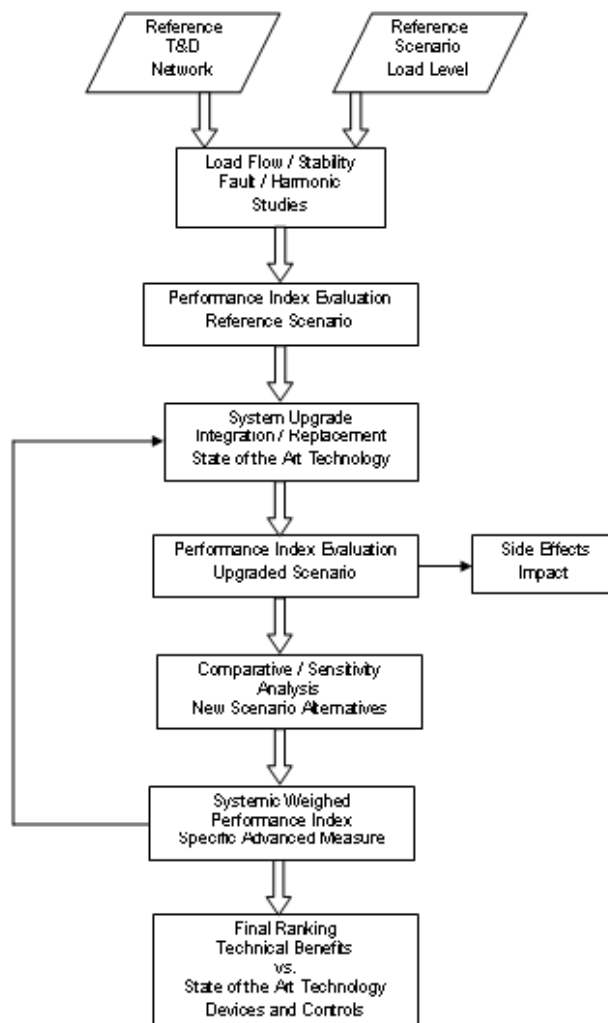
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306 In the steady-state domain, a proposed generalized model is sketched in Figure 3.
307 The insertion of new branches is covered by the triple of arrowed internal passive components,
308 which also account for any replacement/refurbishment performed on existing branches. Series
309 voltages and shunt currents contributions, including Δ (variation) to intend them as
310 modifications of the existing morphology, accomplish all possible contribution of
311 compensating devices, as well as innovative transmission and/or distribution systems.
312 Correspondence to specific state-of-the-art technologies is ensured by functional relationships
313 of mutual dependence between the indicated voltage and current incremental generators.
314 Harmonic models for components replacement or refurbishment simply ask for modification of
315 parameters within available or pre-defined harmonic models. The use of advanced
316 compensations or transmission/distribution innovative forms, whenever converters are
317 committed, requires a general harmonic modeling including multi-frequency voltage and/or
318 current generators.
319 In the end, as far as dynamic models are concerned, if attention is focused on rapid
320 electromagnetic transients, a general set of algebraic differential equations are required to
321 represent both extremely detailed components and fast, dedicated control loops. Conversely,
322 when electromechanical analyses are performed, still a general set of algebraic differential
323 equations are required, this time less devoted to component modeling dynamics (apart for
324 mechanical state variables) and widely concerning control loops at each hierarchical level (with
325 extensive use of transfer functions and non-linearity, whenever present).
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327 IV. THE COMPARATIVE PROCEDURE

328 In this section, the performance indices, the modeling techniques and the network structures
329 previously outlined are employed for assessing benefits and possible troubles related to the use
330 of state-of-the-art technologies in T&D grids.
331 In order to give some driving lines about the technical approach to evaluate both direct and
332 indirect benefits on T&D systems, together with side effects and mitigation, due to state-of-the-
333 art technologies, it is possible to conceive a comparative, selective, and flexible procedure.
334 Comparative: the aim of the procedure is to compare performance indices obtained in a
335 reference operating scenario with those pertaining to upgraded assets including state-of-the-art
336 technology support. As a general remark, several performance indices may be independently
337 affected by upgrading the reference scenario; for instance, the well-known local power factor
338 correction reduces losses and improves voltage profile of the distribution network. In other
339 cases, improving a specific index causes a dependent fall down on some other indices; thus,
340 increasing renewable diffused resource produces a decrement of current flows within the
341 distribution network and consequently reduction of losses (efficiency index) and voltage drops
342 (quality distribution index).
343 Selective: the procedure should allow to create upgraded scenarios, thank to the state-of-the-art
344 technologies, by including, one at each time, either new devices or advanced control strategies.
345 It may be noted that the action could either integrate or replace components or strategies
346 defined in the reference scenario.
347 Flexible: the comparison of performance indices has to be accomplished by a sensitivity
348 analysis to capture the best result. In detail, location and size of advanced equipment must be
349 tested to measure direct advantages. A unifying approach would suggest to normalize benefits
350 to a unitary advanced measure: however, difficulties may arise both in quantifying unitary
351 action and in extrapolating results due to non-linear systems constraints. Moreover, impact of
352 different load profiles and modified generation assessment should be investigated to put into
353 evidence indirect benefits.

354 The fundamental operating steps of the developed procedure are reported in Fig. 4.
 355 It should be highlighted that a sensitivity analysis must be developed in order to define the
 356 optimal set-up. Modified scenarios for analysis should be chosen in such a way to explore a
 357 limited but at the same time, meaningful set of possibilities covering applications of actual
 358 interest. Depending on the specific measure, either analytical or simulation based approaches
 359 may be followed for the analysis; in general a refining optimization process could be adopted to
 360 catch the best measure to grid fitting.
 361 The evaluation of performance indices with and without state-of-the-art technology devices or
 362 control functions makes available evidence of the quantitative impact, together with its
 363 sensitivity, of the selected measure. From a general point of view, a mixed set of indices
 364 variations (positive and negative values) could result from comparison, thus denoting that a
 365 specific advanced provision may, at the same time, favor some operating aspects and worsen
 366 some others.
 367 Consequently, a *weighted average index* should be defined, in order to definitely link an
 368 advanced measure to the performance index overall set. Finally, a ranking process could be
 369 proposed to provide a merit list of the different state-of-the-art advanced solution on T&D
 370 system performance.
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Fig. 4. Performance index evaluation: flow chart of the comparative procedure.

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V. RESULTS

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Once the methodology has been defined, the successive step is calculating the performance indices for each family of T&D state-of-the-art technology in standardized model grids. This is a hard task, which should be unavoidably split in multiple parallel sub-tasks, faced by different and specialized research teams.

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Anyway, an indication on the kind of impact (direct or indirect) provided by the single improving measure on T&D infrastructures can be identified without resorting to any calculations (see Table III).

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TABLE III
IMPACT ON T&D EU ENERGY TARGETS PROVIDED BY THE INTRODUCED ACTIONS

Impact of : Action :	Efficiency	CO₂ Reduction	Renewables	Steady-state quality in T&D	Harmonic quality in distribution	Dynamic quality in transmission	Dynamic quality in distribution
Replacement/ Refurbishment of Power Components	Direct effect (lower losses)	Indirect effect (via more efficiency)	Indirect effect (removal of bottlenecks)	Direct effect (improved parameters)	Indirect effect (improved parameters)	Indirect effect (improved parameters)	Indirect effect (improved parameters)
WAMS/WACS & Upgrading Protection and Control Devices for Communication	Direct effect (flow rescheduling)	Indirect effect (via more efficiency)	Indirect effect (removal of bottlenecks)	Direct effect (regulation)	Indirect effect	Direct effect (improved strategies)	Direct effect (improved strategies)
Increase of Voltage Level of the Power Grid	Direct effect (lower losses)	Indirect effect (via more efficiency)	Indirect effect (removal of bottlenecks)	Indirect effect (reduced drops)	Direct effect (harmonic current sources)	Indirect effect	Indirect effect
Installation of Power Quality Devices (Distribution Networks)	Indirect effect	Indirect effect (via more efficiency)	Indirect effect (support volatile generation)	Direct effect (regulation)	Direct effect (as active filters)	-	Direct effect (as custom power)
HVDC (line and forced commutated)	Direct effect (geographically dependent)	Indirect effect (via more efficiency)	Direct effect (removal of bottlenecks)	Indirect effect (regulation)	Indirect effect (side effect)	Direct effect (dedicated controls)	Direct effect (dedicated controls)
FACTS (Transmission Networks)	Direct effect (flow rescheduling)	Indirect effect (via more efficiency)	Indirect effect (removal of bottlenecks)	Direct effect (regulation)	-	Direct effect (dedicated controls)	-

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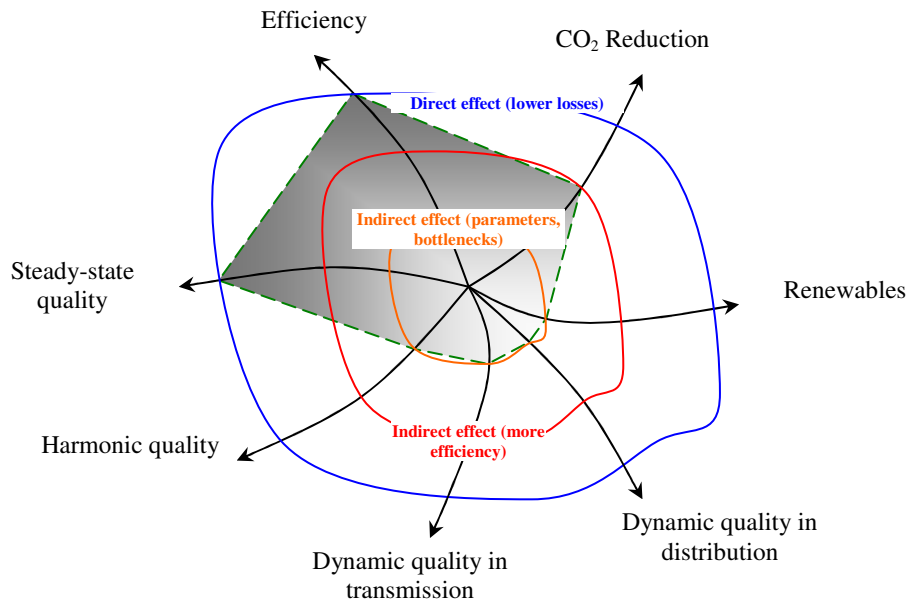
An equivalent, but more explicit, presentation of the expected results of the study is hereafter proposed by means of spider diagrams, reporting in Figures 5 – 10 the effects of each introduced action on the seven targets considered so far.

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Replacement / refurbishment of Power Components



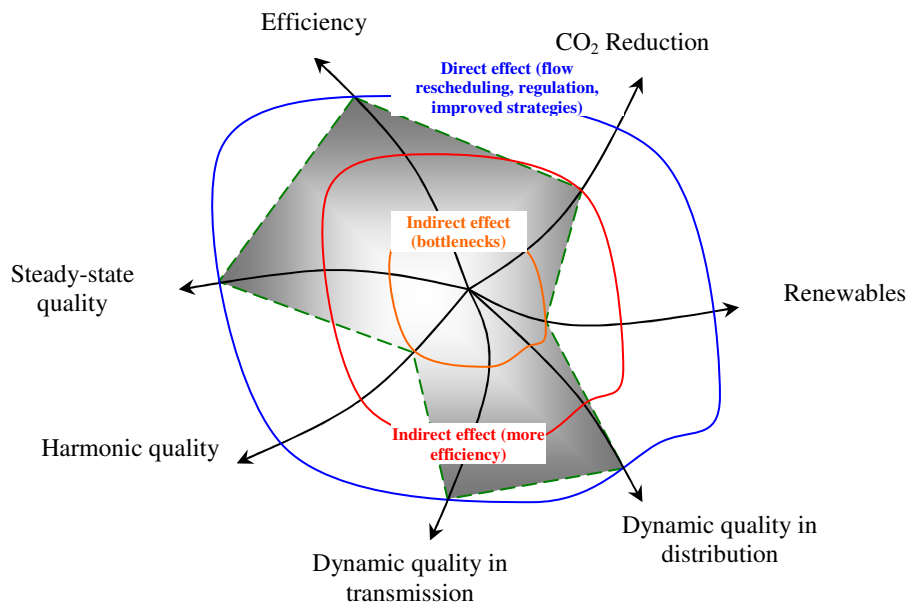
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Fig.5. Spider diagram for the effects of replacement/refurbishment of power components.

WAMS/WACS & Upgrading Protection and Control Devices for Communication



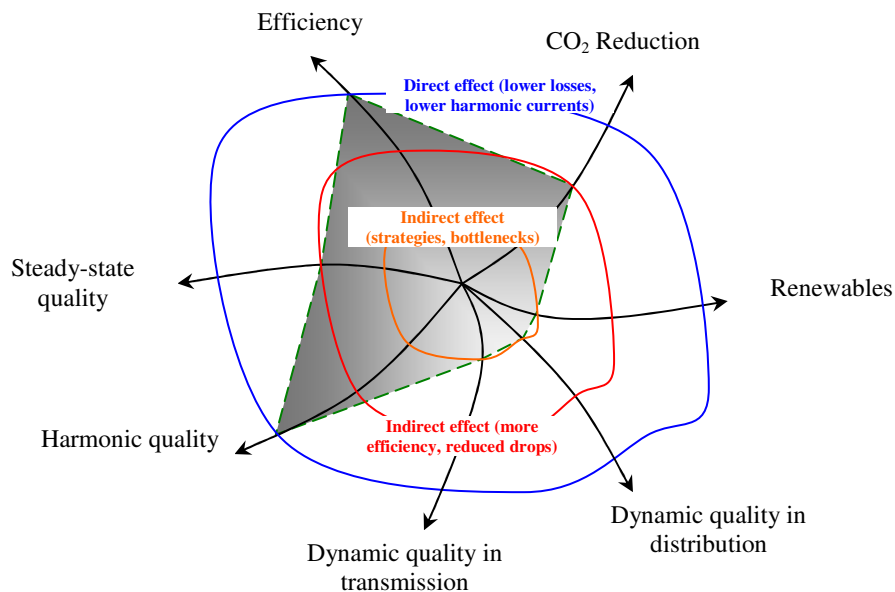
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Fig. 6. Spider diagram for the effects of WAMS/WACS & upgrading protection and control devices for communication.

Increase of Voltage Level of the Power Grid

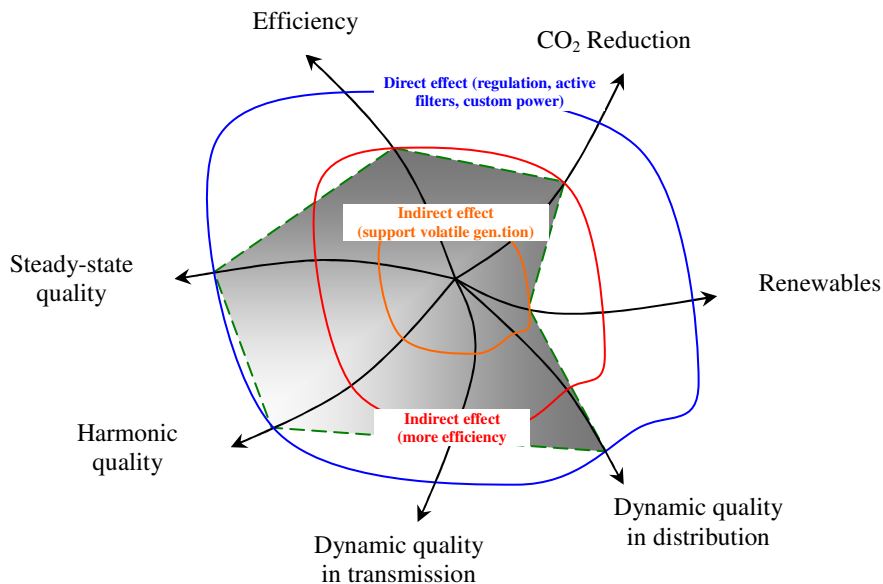


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Fig. 7. Spider diagram for the effects of increase of voltage level of the power grid.

**Installation of Power Quality Devices
(Distribution Networks)**



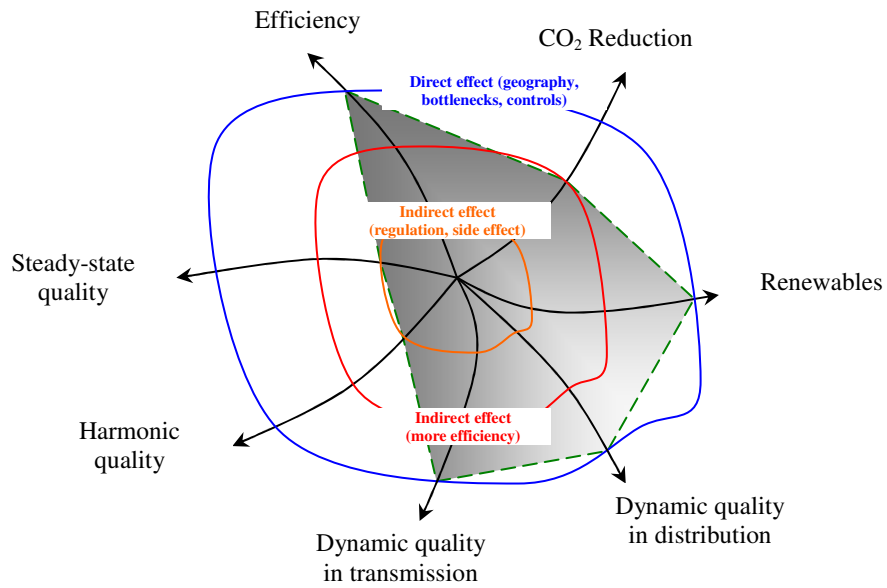
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Fig. 8. Spider diagram for the effects of installation of power quality devices (Distribution Networks).

HVDC (Line and Forced Commutated)



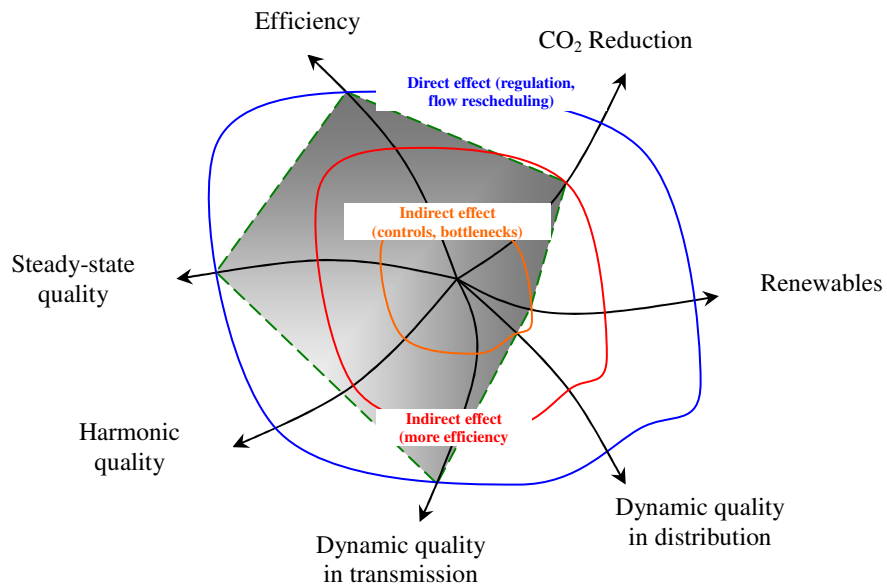
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Fig. 9. Spider diagram for the effects of HVDC (line and forced commutated).

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FACTS (Transmission Networks)



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Fig. 10. Spider diagram for the effects of FACTS (Transmission Networks).

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410 **VI. CONCLUSIONS AND PERSPECTIVES OF FUTURE WORK**

411 In this paper, a general procedure to quantify the possible environmental benefits as well as the
412 power quality improvement provided by the application of modern T&D products and systems
413 on the power grids has been presented. The procedure is based on the definition of suitable
414 performance indices and suitable test networks, where to evaluate such indices. Work is now in
415 progress to perform the identified quantitative and selective analyses to numerically express the
416 effects of each single improving measure on T&D infrastructures. This work is presently split
417 in multiple parallel tasks and will be performed by research teams at different European
418 universities.
419

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